

Fig. 3 Oil flow pattern, $\beta = 40^\circ$, $\alpha = 30^\circ$.

spike and a significant increase in the fluctuating pressures on the flap are typical of the many buzz cases observed.

Hypersonic buzz was first found to be related to angle of attack. With a flap angle of 40° and an angle of attack of 0° , the high-speed schlieren motion pictures indicated that the shock wave and flowfield surrounding the model were generally steady, although tunnel flow fluctuations and wall noise did cause some low-level disturbances. As the angle of attack increased, some unsteadiness appeared, but the level remained very low. As the angle of attack passed through 20° and beyond, the entire scale of the disturbances rapidly changed. The impinging shock (appearing as a white streak in the films) resembled an electric discharge arc as it danced rapidly back and forth along the flap. At the same time, the entire flow structure oscillated wildly. At the maximum angle of attack, 37° , the impinging shock progressed to the forebody and the oscillation amplitudes decreased from their maximum, although they still were large.

Within the confines of a selected range of aerodynamic and geometric parameters, it was observed that the flow underlying the region of a downward deflected flap can be very unstable at hypersonic speeds. Experimental criteria for the existence of large-scale unsteady oscillations were found to be related to the formation of a separation pocket and the presence of multiple shock interactions occurring near the separated shear layer's reattachment point.

Three conditions were required for the onset and continuation of large-scale oscillations: 1) a sizable separation region must develop; 2) the shock resulting from the intersection of the bow

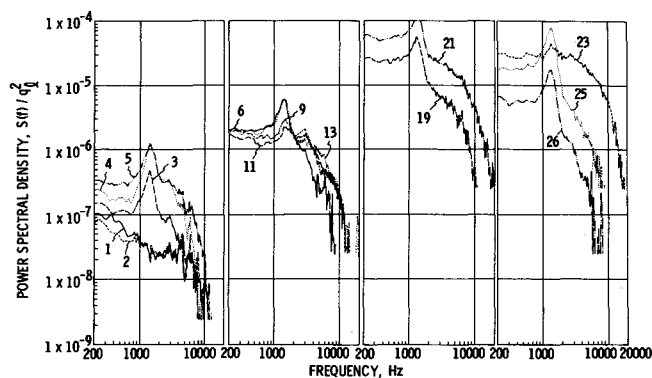


Fig. 4 Surface pressure power spectral densities, $\beta = 40^\circ$, $\alpha = 30^\circ$.

and flap shocks must impinge on either the body or the flap surface; 3) shock impingement must be in close proximity to—or upstream of—the shear layer's reattachment point. Within the flow and geometry conditions tested, this third condition was in itself sufficient for buzz to occur.

Apparently, the proximity of the impinging shock and the reattaching shear layer allow pressure fluctuations, which accompany slight unsteady movements of the impinging shock, to be fed back through the separated pocket. The impinging shock then affects conditions at the separation point and modifies the reattachment position of the separated shear layer. The details of this feedback mechanism are far from understood, and the results do not rule out a role for flap motion (at the flap frequency) in the mechanism. The fluctuations are of sufficient magnitude to be important to the design of a hypersonic vehicle with a separated pocket, and experience from this study should aid in establishing general design criteria for such hypersonic vehicle configurations.

References

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